

*Ice formation in supercooled turbulent water*  
*A parametric study*

Piero Olla

ISAC-CNR & INFN Sez. Cagliari  
I-09042 Monserrato (CA) ITALY

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## *Frazil ice and grease ice*

- ▶ Ice production in polar seas usually takes place in the presence of strong winds.
- ▶ In the initial stage, small “frazil” ice crystals are generated at the water surface, where they accumulate to form a slurry of greasy appearance: the so called grease ice.
- ▶ Only later does grease ice thicken enough to form more compact objects and hence a continuous solid layer.



Picture of grease ice cover in the Northern Barents Sea.

- ▶ Frazil ice formation is a violent process and is responsible of strong increase of heat exchange between the ocean and the atmosphere.



## *Processes involved in the formation of frazil ice.*

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- ▶ Ice seeds are continuously generated at the water surface (first nucleation), and grow to mm size in the presence of strong overcooling.
- ▶ Additional seeds are generated by breaking of crystals from mutual collisions in the grease ice layers (secondary nucleation).
- ▶ Part of the crystals get transported down the column by turbulence; another portion may be blown away by the wind; the rest accumulates in the form of grease ice.

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*“Complicated” problem with many effects under poor control:*

- ▶ The growth of the crystals in a complex environment is very difficult to model.
- ▶ It is difficult to estimate entrainment of frazil crystals in the underwater turbulence.



## What do we know

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- ▶ Ice grows in overcooled condition:  $T - T_i < 0$ .
- ▶ The freezing temperature decreases with salinity,  $T_i = T_{iB} - a_S S$  ( $S$  is the increase of salinity with respect to the background  $S_B$ ).
- ▶ Latent heat  $\mathcal{L}$  is released in the liquid phase during freezing.
- ▶ Most of the salt in the crystals is expelled to the liquid phase.



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- ▶ Water gets warmer and saltier. Imposing  $T - T_i = 0$  allows us to get the ice fraction at saturation

$$C = (\rho_w/\rho_i)(a_S S_B + \mathcal{L}/c_P)(T_{i0} - T_0).$$

- ▶ It can be seen that the effect of the increase of  $T$  dominates over that of  $S$  during the process.
- ▶ For  $T_{i0} - T_0 = 0.1^\circ\text{C}$ , we get  $C \approx 10^{-3}$ .



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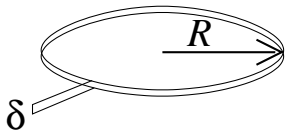
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*Is it big or is it small?*

### Typical geometry of frazil crystal



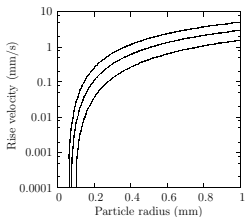
- ▶ Radius of ripe crystal  $R \approx 1$  mm,  $\delta/R \approx 0.01$ .
- ▶ Effective volume of the crystal  $\approx R^3$ .
- ▶ Volume fraction occupied by ice  $\approx \delta/R$ .

Sketch of a frazil crystal

- ▶ This leads us to expect  $C_{grease} \approx \delta/R \approx 0.01$ .
- ▶ A mixture with smaller crystals would lead to a mortar-like, more compact assembly with higher  $C$ .
- ▶ Transport processes are obviously important (you need them to get  $C \approx C_{grease}$ ).



## Rise velocity of the frazil crystals



Plot of frazil crystal rise velocity for different aspect ratios. From bottom to top,  $\delta/R = 1/100$ ,  $1/50$ ,  $1/25$ .

We are in a forced turbulence situation, induced by strong wind at the water surface ( $u^{wind} \approx 10$  m/s, leading to a friction velocity  $u_* \approx 3$  cm/s underwater). In the first approximation we can disregard the rise velocity of the crystals.



## Turbulence structure

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### Navier-Stokes dynamics (Boussinesq)

$$(\partial_t + \mathbf{u} \cdot \nabla) \mathbf{u} + \frac{1}{\rho_w} \nabla P = \nu \nabla^2 \mathbf{u} - \hat{\alpha}_T T + \hat{\alpha}_S S - \hat{\alpha}_C C,$$

$$\hat{\alpha}_T \simeq 3.79 \cdot 10^{-4} \text{ m}/(^{\circ}\text{C s}^2); \quad \hat{\alpha}_S \simeq 7.7 \cdot 10^{-3} \text{ m}/(\text{psu s}^2);$$

$$\hat{\alpha}_C = g(1 - \hat{\rho}) \simeq 1 \text{ m/s}^2$$

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- ▶ We can estimate the contribution to buoyancy from an increase  $\delta C$  in the ice volume fraction:

$$\delta T \sim \frac{\rho_i \mathcal{L}}{\rho_w c_P} \delta C \quad \text{and} \quad \delta S \sim \frac{\rho_i S_B}{\rho_w} \delta C, \quad \text{leading to}$$

$$\frac{\hat{\alpha}_T \delta T}{\hat{\alpha}_C \delta C} \simeq 0.06 \quad \text{and} \quad \frac{\hat{\alpha}_S \delta S}{\hat{\alpha}_C \delta C} \simeq 0.24.$$

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- ▶ Ice dominates salinity, which dominates temperature.



## *The mechanical turbulence layer*

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- ▶ The Obukhov depth  $L$  can be determined from the heat flux  $\Phi_T$  at the surface. Estimates during ice formation range from  $2.5 \cdot 10^{-5} \text{ }^\circ\text{C m/s}$  to  $2.5 \cdot 10^{-4} \text{ }^\circ\text{C m/s}$ . What we get depends on how much ice forms at the surface.



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- ▶ If all the ice were transported down the column,  $L$  would be further reduced, with possibility of a double convection regime at  $z < -L$ .





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- ▶ Simple parametrization of ice production:

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- ▶ Two limit scenarios, depending on ice entrainment at the surface:
  - ▶ Little ice transported down the column. All ice melts at  $z < -L_o$ . Little effect on  $T_o$ .
  - ▶ Lots of ice transported down the column.  $T_o \rightarrow 0$ , with little effect on  $C$ . Ice reaches bottom of mechanical turbulent layer.

- ▶ A situation in which lots of ice get transported down the column is observed in LES (Matsumura & Ohshima, Ann. Glaciol. 2015) as well as in older 1D models (Omstedt and Svensson, J. Geophys. Res. 1984).
- ▶ Condition for ice production to dominate overcooling down in the column (assuming stationarity):  $T_o^* \ll \hat{L}C_*$ , which implies  
**sensible heat flux  $\ll$  latent heat flux from ice transport.**
- ▶ A similar situation holds when the ice remains at the surface: most heat lost to the atmosphere is in this case latent heat from grease ice formation.



## Latent heat vs sensible heat fluxes

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- ▶ A similar situation holds when the ice remains at the surface: most heat lost to the atmosphere is in this case latent heat from grease ice formation.
- ▶ The sensible heat flux, however, cannot be zero.



## Estimate of the sensible heat flux

- ▶ We can decompose the temperature and salinity fields  $T$  and  $S$  in an overcooling component  $T_o = T - T_{iB} + a_S S$  and a neutral component  $T_n = T - T_{iB} - cS$ ,  $c = \hat{L}/S_B$ , which is purely advected with no influence to and from ice formation.
- ▶ From here, we can express the heat and salinity fluxes as

$$\Phi_T = \Phi_{T_o} + (a_S/c)\Phi_{T_n} \quad \text{and} \quad \Phi_S = \frac{\Phi_{T_o} - \Phi_{T_n}}{a_S + c},$$

where  $\Phi_{T_n}$  is conserved.

- ▶  $\Phi_T(0)$  contains both latent and sensible heat fluxes; from  $\Phi_S(0) = 0$ , we get  $\Phi_T(0) = (1 + a_S/c)\Phi_{T_n}$ .
- ▶ At sufficient depth,  $\Phi_T = \Phi_T^{\text{sensible}} > (a_S/c)\Phi_{T_n}$  (fluxes positive defined upwards).
- ▶ This gives

$$\frac{\Phi_T^{\text{sensible}}}{\Phi_T^{\text{latent}}} > \frac{a_S}{c - a_S} \simeq 0.1.$$



## Conclusions

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- ▶ Qualitative description of processes taking place in the turbulent column during ice formation.
- ▶ Identification of a set of key aspects to further investigate to obtain a proper physical description of what is going on:
  - ▶ Entrainment rate of ice crystals on top of the column.
  - ▶ Evaluation of the effective diffusivity in the grease ice layer.
  - ▶ Evaluation of the ice formation rate within the grease ice layer.
  - ▶ Investigation, possibly with LES, of the ice dynamics at and below the Obukhov depth.